

Corrosion Protection of Transport Vehicles by Nanocoating of Decahydrobenzo[8]annulene-5,10-dihyrazone in Corrosive Environments and Weather Change

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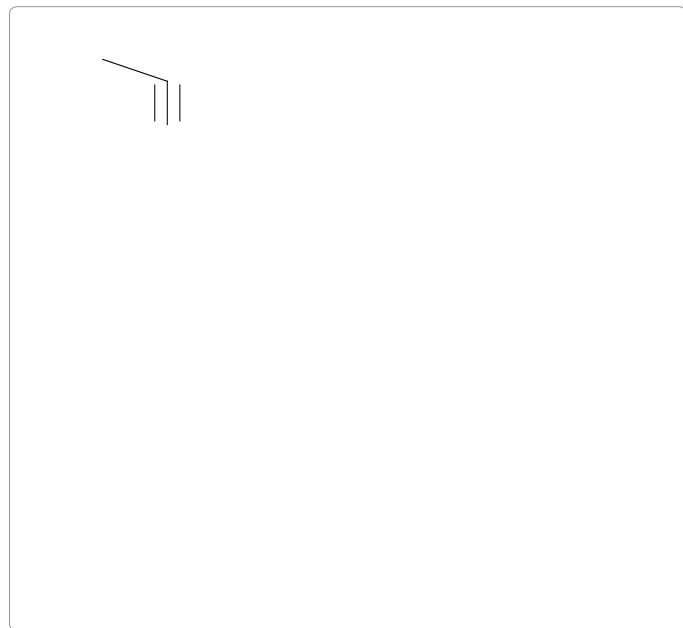
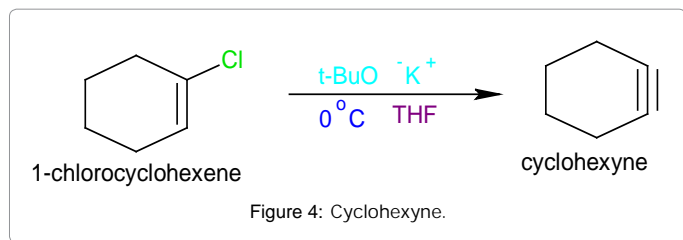
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mode of failure of coated steel surfaces. The detailed mechanisms are unknown, but in an air saturated electrolyte disbanding is usually caused by the oxygen reaction and it is the high pH generated by this reaction that is considered to be most important [14].

The aim of this investigation has been to study the cathodic reaction on coated steel surfaces and to see if there is any connection between the rate of this reaction and the ability of a coating to protect against corrosion.

Although the combined application of plastic coating [15] and cathodic protection has become a widespread and general technology for preventing corrosion on buried steel pipelines, corrosion failures are still occasionally experienced, among others under disbonded coatings. The significance of coating disbonding has increasingly been realized since the first recognition of disbonding as a possible origin



of decahydrobenzo[8]annulene-5,10-dihydrazone 85% was obtained (Figures 10-13).

Results and Discussion

The corrosion rates of epoxy-coated stainless steel, Nanocoated of decahydrobenzo[8]annulene-5,10-dihydrazone and SiC filler were calculated by equation $K=13.56 \times (W/ADt)$ and their results are

written in Table 1. It was observed in absence of coating the corrosion rate of epoxy-coated stainless steel increased but these values were reduced in presence of nanocoating and filler compounds. The results of Table 1 indicate that without coating corrosion rate of epoxy-coated stainless steel enhance at lower temperature to higher temperature. These values minimize with nanocoating and filler compounds. Figure 14 plotted between corrosion rate $K(\text{mmpy})$ vs. $t(\text{hrs})$ indicates that corrosion rate increased with exposure times duration were low. Nanocoating and filler compounds reduced corrosion rate as shown in Figure 14. The corrosion rate of material is function of time, if material is exposed in atmosphere in a longer duration without any protective substance, their corrosion rate accelerate. It is very difficult to prevent the corrosion of epoxy-coated stainless steel corrosion but this technique give good results in above corrosive medium and weather conditions (Table 1 and Figure 14).

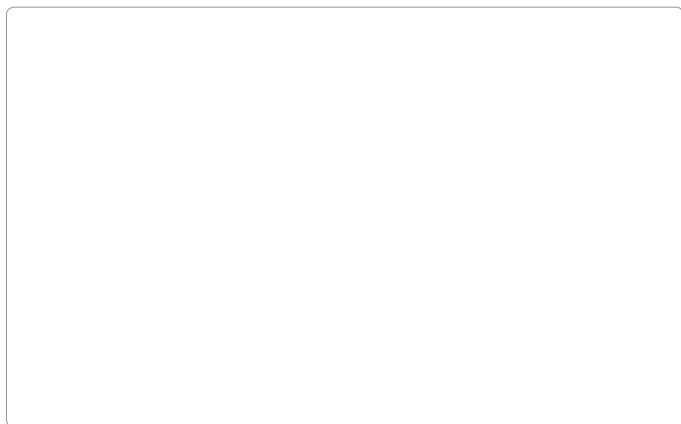
Corrosion rates of epoxy coated stainless steel, nanocoated of decahydrobenzo[8]annulene-5,10-dihydrazone and SiC filler were calculated at different temperatures and their values are mentioned in Table 1. Figure 15 plotted between $\log(K)$ vs. $\log(t)$ which indicated a straight line that the corrosion rate of epoxy-coated stainless steel reduced with nanocoating and filler material from lower to higher temperatures. Its values enhance without coating. Decahydrobenzo[8]annulene-5,10-dihydrazone is an electron rich compound which adhere on the surface of epoxy-coated stainless and SiC filler blocks porosities of nanocoated material. Figure 15 shows that nanocoating and filler compounds reduced corrosion rate from lower to higher temperatures (Figure 15).

The results of Table 1 noticed that nanocoating and filler compounds enhanced the values of $\log(i_{corr})$ at lower to higher temperature. Figure 16 drew between $\log(i_{corr})$ vs. $1/T$ found to be straight line which indicated that both compounds were increased its values as temperatures rising. The values $\log(i_{corr})$ of both compounds were shown that they mitigated corrosion rate and enhanced stability of surface barrier (Figure 16).

The surface coverage area (%) was covered by decahydrobenzo[8]annulene-5,10-dihyrazone and SiC filler at different temperatures

N NH

N NH₂



porosities of nanocoating compound and produced non-permeable thin film layer on the surface of base material. This barrier layer stops osmosis or diffusion process of corrosion pollutants (Figure 2).

Nanocoating compound decahydrobenzo[8]annulene-5,10-dihyrazone and SiC film surface thin film formation, bond formation, adsorption properties, types of reaction, stability and permeability barrier were studied by activation energy, heat of adsorption, energy, enthalpy and entropy. Activation energy of decahydrobenzo[8]annulene-5,10-dihyrazone and SiC film were calculated by Arrhenius equation $\ln k = \ln A - \frac{E_a}{RT}$ and Figure 2 plotted between $\log k$ vs $1/T$ and their values are mentioned in Table 2. The results of Table 2 show that without coating activation energy values were high but after coating its values decreased as temperature enhanced. These results indicate that nanocoating and film compounds formed chemical bonding with base material. Heat of adsorption for nanocoating and film compounds were determined by equation $\log \left(\frac{1}{1-\theta} \right) = \log \left(\frac{A}{q} \right) - \frac{q}{2.303RT}$ and Figure 3 and their values were expressed in Table 3. Heat of adsorption values found to be negative in both compounds confirmed that nanocoating and film compounds attached with electrode coated stainless steel by chemical bonding. The negative sign of energy indicated that nanocoating of decahydrobenzo[8]annulene-5,10-dihyrazone and SiC film developed chemical bonding during

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6. 'HYHFL + \$KPHWWL * (UVR] 0 ORGL ĩ HG V WIVSUZHGH VQ, & HR UMRK r RQ (2009) LAFrmine self-assembled monolayers mechanical and thermal properties evaluation. *Prog Org Coat* 73: 1-7. against copper corrosion and synergitic effect of iodide ion. *J Appl Electrochem* 39: 1193-1198.
7. Genzer J (2005) Templating Surfaces with Gradient Assemblies. *J of Adhesion* 81: 417-435.
8. Leon-Silva U, Nicho ME (2010) Poly(3-octylthiophene) and polystyrene blends thermally treated as coating for corrosion protection of stainless steel 304. *J Solid State Electrochem* 14: 1487-1497.
9. Baier RE (2006) Surface behaviour of biomaterials: Surface for biocompatibility, *J. Mater. Sci Mater Med* 17: 1057-1062
10. Rao BVA, Iqbal MY, Sreehar B (2010) Electrochemical and surface analytical studies of the self assembled monolayer of 5-methoxy-2-(octadecylthiol) benzimidazole in corrosion protection of copper. *Electrochim Acta* 55: 620-627.
11. Liu XY, Ma HY, Miao S, Zhou M (2009) Self-assembled monolayers of stearic imidazoline on copper electrodes detected using electro chemical measurement XPS, molecular simulation and FTIR. *Chinese Sci Bull* 54: 374-381.
12. Liao QQ, Yue ZQ, Zhu ZW, Wang Y, Zhang Y, et al. (2009) Corrosion inhibition effect of self-assembled monolayers of ammonium pyrrolidine dithiocarbamate on copper. *Acta Phys Chin Sin* 25: 1655-1661
14. Ghareba GS, Omanovic S (2010) Interaction of 12-aminododecanoic acid with a carbon steel surface: Towards the development of green corrosion inhibitors. *Corrosion Sci* 52: 2104-2113.
15. Sahoo RR, Biswas SK (2009) Frictional response of fatty acids on steel. *J Colloid Interf Sci* 333: 707-718.
16. Raman R, Gawalt ES (2007) Selfassembled monolayers of alkanolic acid on the native oxide surface of SS316L by solution deposition. *Langmuir* 23: 2284-2288.
17. Li DG, Chen SH, Zhao SY (2006) The corrosion inhibition of the self-assembled \$X DQG \$J QDQRS DUWLF OHV ĩ OPV RQ WKH VXU>ñ, 'H CEG e5: 12630-2640