Iran is one of the most seismic countries in the world, a lot of earthquakes occur in Iran every year. Some actions and researches have been done about Earthquake Disaster Risk Management feld since 1990 after large earthquake of Manjil-Rudbar in Iran. One of the main subjects of Earthquake Disaster Risk Management is Community base Disaster risk Management (CBDRM). This paper presents the idea of Earthquake Disaster Management Multipurpose Complex (EDMMC) with self-help neighborhood approach that has been proposed for making CBDRM feasible in each neighborhood of a large city like Tehran, The case study is Youssef Abad-region6-Tehran. Furthermore, in structural Design, the seismic behavior of Earthquake Disaster Management Multipurpose Complex (EDMMC) was evaluated using dynamic nonlinear analysis. In total, three different structures (the building of a training complex with a typical foundation (M_1), the steel building of the training complex with a LRB base-isolator (M_2), and the steel building of the training complex with rocking structural systems (M_3)) were studied applying three earthquakes of Northridge, Kobe, and Chi-Chi. Several seismic parameters were also evaluated including time history of displacement (displacement time), time history of base shear (force-time), and the hysteresis diagram (force-displacement). The results indicate the appropriate function of the selected M_2 and M_3 model in controlling and decreasing the seismic responses of the structure.

billions of dollars and oen constitute a large percentage of the gross national product of the country aected. Additionally, the damage caused by earthquakes is almost entirely associated with manmade structures. As in the cases of landslides, earthquakes also cause death by the damage they induce in structures such as buildings, dams, bridges and other works of man. Unfortunately many of earthquakes give very little or no warning before occurring and this is one of the reasons why earthquake engineering is complex [1,2].

Also buildings, which are tall in comparison to their plan area, will generate high overturning moments while buildings with large plan

the complexity of the active control needed. However, it couples vibration modes (natural frequencies) which have been calculated for an un-damped system [2-4].

Subramani et al. presented an overview of the present state of base isolation techniques with special emphasis and a brief on other techniques developed world over for mitigating earthquake forces on the structures. e e ects of base isolation on structures located on so soils and near active faults are given in brief. Simple case study

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Workshops, Workshops about Earthquake, Gymnasium, Conference Hall, Court Yard, Storage.

• A er earthquake: Temporary Accommodation, Emergency

Drawing

Drawings include some plans (before and a er earthquake), dimension plans, elevations and sections plans (Figures 16 and 17).

Building materials

is section discusses ETFE, PTFE and CRFC that are considered as nishing materials for this project (Figure 18).

GFRC as nishing: Glass Fiber Reinforced Concrete (GFRC) is one of the most innovative construction materials available and

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Building Materials.



following earthquakes:

- 1- Kobe earthquake (1996)
- 2- Northridge earthquake (1995)
- 3- Chi Chi earthquake (1999).

e temporal step and the total time of the record of each accelerations have been shown in Table 1.

Drawing the acceleration diagram- time of acceleration

According to 2800 standard criteria, a er selecting the related earthquakes, all of acceleration values in certain temporal steps are obtained by introducing the earthquake's acceleration pair to the so ware and are drawn by the so ware. In this way, the maximum acceleration of the acceleration pair (PGA) is obtained. It is worth mentioning that scaling acceleration pair via SEISMOSIGNAL so ware is used for reading and drawing the acceleration of the selected earthquakes.

Scaling acceleration to the maximum value

e rst stage involves scaling the obtained acceleration from the so ware to the maximum value which equals *g* acceleration. To this aim, we should nd a number so that the obtained PGA at the rst stage multiplied by that number equals *g* acceleration. We can show it by the following relation:

eg/PGA	(1)
- <u>5</u> /1 0/1	(1)

In this relation, equals the scale factor that scales the accelerations to its maximum value (Table 2).

As shown in Figure 23, the value of acceleration is scaled to its maximum value, i.e. g (Figure 24).

Nonlinear dynamic analysis (time history)

Steel structure with typical foundation (M,): In nonlinear time

Temporal step	0.005	0.01	0.02
Total time	90	24	48

The temporal step and the total time of accelerations	The	e temporal	step and	the total	time of	accelerations
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		Coef f cient
Kobe	0.599 g	1.669
Northridge	0.879 g	1.138
Chi Chi	0.474 g	2.109

FTFF Film

Lists PGA and coeff cient for each accelerogram.



ETFE Section [13].

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history analysis, the load was applied on the structure as acceleration in both directions of X and Y by Kobe, Northridge, and Chi-Chi earthquakes. e results obtained by modeling and analyzing are shown in Figures 25 and 26.

We rst evaluate changes in displacement and force exerted on the structure both in X and Y directions considering changes in time (Figures 27, 28, Tables 3 and 4).

Tables 5 and 6 show the maximum force caused by the mentioned earthquakes.

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Kobe	Kobe Chi-Chi Northridge			
7.6 7.9 5.8				
MAX Displacement=7.9 mm				
Maximum displacement in Y-direction for M_2 Model.				

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the structure both in X and Y directions considering changes in time (Figures 39 and 40). Tables 11 and 12 list the maximum displacements over time caused by the earthquakes.

Tables 13 and 14 show the maximum force caused by the mentioned earthquakes.

e maximum force in X happened due to Kobe earthquake which is 885 tones. Northridge earthquake caused the maximum force in Y, with a value of 1090 tones. A er representing diagrams of changes in displacement and force exerted on the structure (displacement-time and force-time) both in X and Y directions considering changes in time and interpreting the results, we will evaluate hysteresis diagrams (Figures 41 and 42).

As shown in Figures 41 and 42, the structure did not enter the nonlinear state by the three earthquakes and the structure displacement remained in the elastic state. Given that the area under the hysteresis diagram represents the absorbed energy, Chi-Chi had the maximum energy loss along X and Y, respectively.

In general, the area under the hysteresis diagram represents the amount of energy absorbed by the structure under the load. On this basis and considering Figure 41, we can conclude that M_3 absorbed the maximum amount of energy and entered the nonlinear state under Chi-Chi earthquake while in X, the structure did not enter the



Tehran, e case study is Youssef Abad-region6-Tehran and then is designed one EDMMC with high performance of architectural and structural earthquake resistance design, that has di erent function before and a er earthquake. Before earthquake EDMMC is a public school and a er earthquake EDMMC allows neighborhood to help wounded people before coming of rescue and relief team and reduces the casualty of an earthquake disaster. But, in structural Design, the seismic behavior of Earthquake Disaster Management Multipurpose Complex (EDMMC) was evaluated using dynamic nonlinear analysis. In total, three di erent structures (the building of a training complex

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area under the hysteresis diagram represents the absorbed energy, Chi-Chi had the maximum energy loss along X and Y, respectively.

• M_3 absorbed the maximum amount of energy and entered the nonlinear state under Chi-Chi earthquake while in X, the structure did not enter the nonlinear state by the three earthquakes and showed far less plasticity than other available earthquakes in Y.

• In the hysteresis diagram of M_3 in Y, the only important point was the nonlinear behavior of the structure under Chi-Chi and earthquake that absorbed a considerable amount of energy compared to Northridge and Kobe earthquakes.

Comparing displacements in X and Y, we found that the maximum displacement in X (8.1 mm) was experienced by M_2 and caused by Chi-Chi earthquake. In addition, the maximum displacement in Y was 7.9 mm, experienced by M_2 (steel foundation with LRB base isolator) and caused by Chi-Chi earthquake. As discussed, the maximum displacement of M_2 in Y under Chi-Chi earthquake is about 2.5% more than the maximum displacement in X.

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